Appendix A Soil Investigation and Railway Crossing



May 25, 2022

Calgary, AB T2P 4Z4

FILE: 734 -2200120200-PAL-G0001-01
Canadian Pacific Railway
Via Email: <u>Utilities_RequestsCanada@cpr.ca</u>
Suite 500 Gulf Canada Square
401 9th Avenue SW

Attention: Mr. Jack Carello

Subject: Request for Railway Crossing Permit

Midland Street near Saskatchewan Avenue, Winnipeg, Manitoba

We are requesting a permit for a buried watermain pipeline crossing a CPR spur line on Midland Street near Saskatchewan Avenue in Winnipeg, Manitoba. The work is part of the City of Winnipeg 2022 Watermain Renewals (Contract 10) and involves the installation of a 300mm diameter watermain to replace the existing older watermain that is being abandoned. It is anticipated the construction to install the watermain crossing at the CPR spur line will occur in the fall of 2022, pending permit. The spur line runs in a west-east direction crossing Midland Street in the area under review for permit.

Applicant Information:

Tetra Tech Canada Inc. Indira Maharaj, P.Eng. 400-161 Portage Avenue East Winnipeg, MB R3B 0Y4 Phone: 204-954-6844 indira.maharaj@tetratech.com

Utility Owner:

City of Winnipeg Ryan Lucky, P.Eng. 110-1199 Pacific Avenue Winnipeg, MB R3E 3S8 112-1199 Pacific Avenue Winnipeg, MB R3E 3S8 (invoicing)

Phone: 204-986-2538 ryanlucky@winipeg.ca

Information requested for invoicing or otherwise, should reference the City of Winnipeg 362-2022 Bid Opportunity, 2022 Watermain Renewals Contract No 10. The agreement should be sent to the applicant (which is also the contract administrator).

Emergency phone number (utility break or damage): 204-986-2626

The City of Winnipeg also has a 311 service.

CONFIDENTIAL - ISSUED FOR USE

The watermain crossing uses a casing pipe that has been designed to the guidelines specified in the AREMA Manual of Railway Engineering, Chapter 1, Part 5, Pipelines. An information table for the crossing (based on AREMA Table 1-5-6) is attached within the attached sketch along with the construction drawing.

If you have any questions or concerns, please do not hesitate to contact the undersigned.

Respectfully submitted, Tetra Tech Canada Inc.

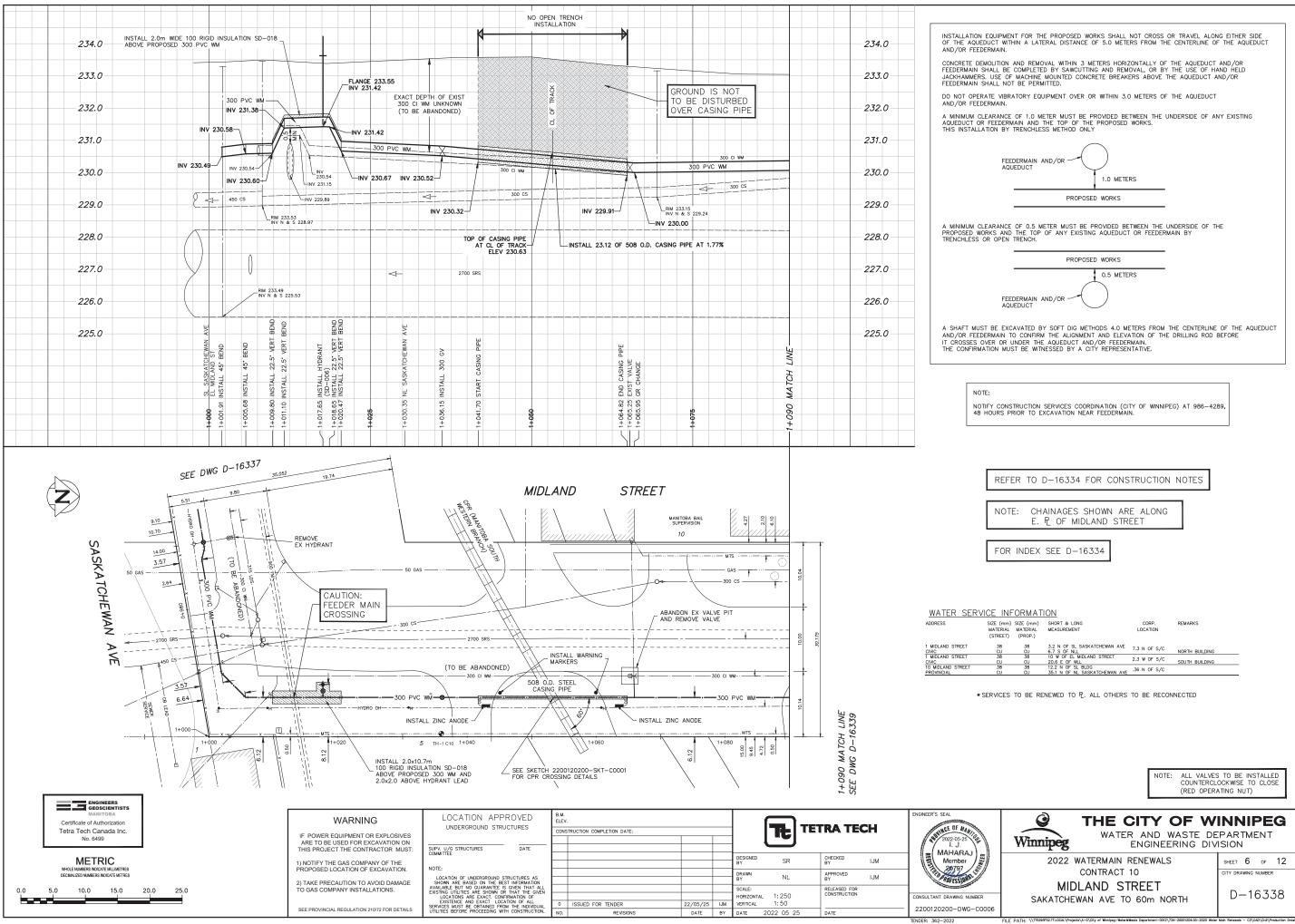
FILE: 734 -2200120200-PAL-G0001-01 FILE: 734 -2200120200-PAL-G0001-01 FILE: 734 -2200120200-PAL-G0001-01 FILE: 734 -2200120200-PAL-G0001-01

Prepared by: Indira Maharaj, P.Eng. Senior Project Engineer indira.maharaj@tetratech.com

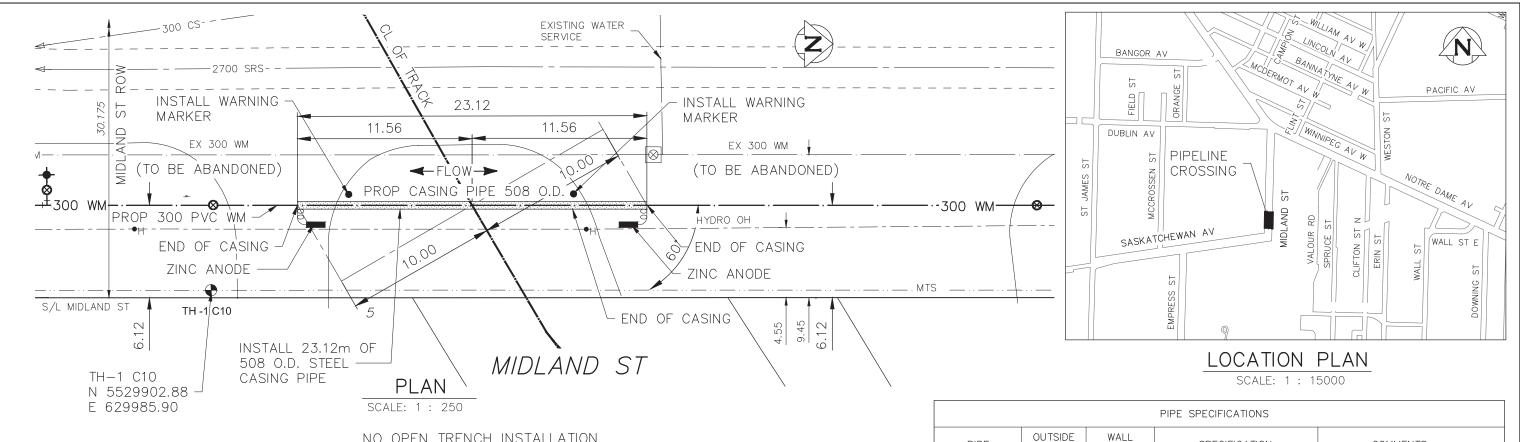
IM/km

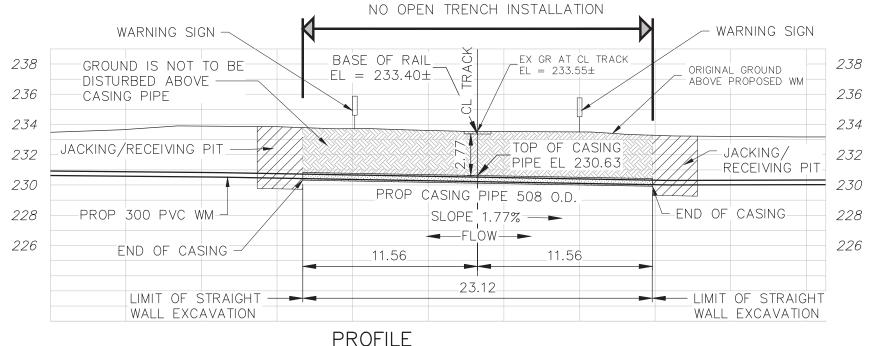
Attachments: WM Crossing on Midland Street for CPR Approval (2200120200-SKT-C0001)

Drawing No 2200120200- DWG-C0006 (City Drawing No D-16338)



FILE NAME: C1003-C1007 2200120200-DWG-C0003-7 Saskatchewan_Midland.dwg





HOR & VERT SCALE: 1: 250

PVC DR 18 BELL & SPIGOT WORKING PRESSURE - 450 kPa/ CARRIER PIPE 335MM 19MM TESTED AT 1034 kPa (WATERMAIN) 508MM CARBON STEEL ASTM A53 TRENCHLESS INSTALLATION CASING PIPE 15MM SCHEDULE 40 - JOINT WELD SS BANDS, POLYMER YES SEE NOTES: MATERIAL 3. SPACERS RUNNERS (APS MODEL SSI) RUBBER END SEALS YES SEE NOTES: MATERIAL 4. (APS MODEL AW) YES SEE NOTES: MATERIAL 5. CATHODIC PROTECTION 10.9 kg ZINC ANODES

SPECIFICATION

COMMENTS

CONSTRUCTION NOTES:

- 1. CONSTRUCTION IN ACCORDANCE WITH TRANSPORT CANADA STANDARD (TCE-10)
- 2. CASING PIPE WILL BE INSTALLED USING TRENCHLESS METHODS BY HORIZONTAL EARTH CORING.
- 3. THE WATERMAIN PIPE WILL BE INSERTED INTO THE CASING PIPE COMPLETE WITH SPACERS AND END SEALS.
- 4. EMERGENCY VALVE LOCATIONS FOR THE 300mm WATERMAIN (25.8 M NORTH & 5.6 M SOUTH FROM CASING PIPE END POINTS).

DESIGN NOTES:

- CROSSING TO BE DESIGNED, CONSTRUCTED, MAINTAINED AND OPERATED IN ACCORDANCE WITH TRANSPORT CANADA STANDARD (TCE – 10), STANDARDS RESPECTING PIPELINE CROSSING UNDER RAILWAYS
- 2. THE WATERMAIN CROSSINGS UTILIZE CASING PIPES DESIGNED TO THE GUIDELINES SPECIFIED IN THE AREMA MANUAL OF RAILWAY ENGINEERING CHAPTER 1 PART 5 "PIPELINES".
- 1. CARRIER PIPE POTABLE WATER PIPE PVC AWWA C-900 CLASS 150 (DR18)
- 2. ENCASEMENT PIPE SHALL CONFORM TO ASTM A53 STEEL PIPE, ASTM SPECIFICATIONS A134 MILD CARBON STEEL, A139, GRADE B. BUTT WELD JOINTS SHALL HAVE A MINIMUM THICKNESS OF 13mm REGARDLESS OF DIAMETER. NO COATING

MATERIALS:

- 3. ENCASEMENT PIPE SPACERS SHALL BE 200MM WIDE, HEAVY DUTY TWO PIECE STAINLESS STEEL BANDS WITH 25mm WIDE BY 75mm SPACERS, EQUAL TO ADVANCE PRODUCTS AND SYSTEMS INC. (APS) MODEL SS18.
- 4. ENCASEMENT PIPE SEALS SHALL BE WRAPAROUND RUBBER WITH STAINLESS STEEL BAND CLAMPS AND WATERPROOF MASTIC SEALS SPACERS EQUAL TO ADVANCE PRODUCTS AND SYSTEMS INC. (APS) MODEL AW OR AZ.
- 5. SACRIFICIAL ANODE 10.9 kg ZINC ANODES AT EACH END OF CASING PIPE.



PIPE

DIAMETER

THICKNESS

Winnipeg WATER AND WASTE DEPARTMENT



DRAWING DESCRIPTION

WM CROSSING ON MIDLAND STREET FOR CPR APPROVAL

AUTHORIZED I	BY: IIM	CLIENT DRAV	WING NO.		
	-5	1			
DATE:	22/05/11				
	22/03/11				
DESIGNED BY:	CID	DRAWN BY:	NIT /CID	DRAWING NO.	REV.
	SJR		NL/SJR		
REVIEWED BY:	113.6	SCALE:	1 250	2200120200 CIZT C0001	0
	IJМ		1:250	2200120200-SKT-C0001	l U



DYREGROV ROBINSON INC. 1692 Dublin Ave #1, Winnipeg, MB, Canada R3H 1A8 204.632.7252 DRIGEOTECHNICAL.CA

May 19, 2022 File No. 224594

Tetra Tech Canada Inc. 400 - 161 Portage Avenue East Winnipeg, MB R3B 0Y4

Attn: Indira Maharaj, P. Eng.

RE: City of Winnipeg – Watermain Renewals - Contract 10 Geotechnical Investigation

As requested, Dyregrov Robinson Inc. (DRI) has undertaken a geotechnical investigation near the Canadian Pacific Railway (CPR) crossing on Midland Street in Winnipeg, MB where a new watermain will be installed below the CPR Right-of-Way for the City of Winnipeg Watermain Renewals (Contract 10) project. The purpose of the investigation was to explore the subsurface conditions in the area of the proposed watermain crossing on Midland Street. The work was authorized by Indira Maharaj of Tetra Tech Canada Inc. on March 30, 2022.

1) Proposed Development and Site Conditions

Based on the attached drawing from Tetra Tech, titled "WM Crossing On Midland Street For CPR Approval", we understand that a 508 mm OD casing pipe for the watermain crossing will be installed across the CPR Right-of-Way on the east side of Midland Street using trenchless methods by horizontal earth coring. A 335 mm diameter watermain carrier pipe will be inserted into the casing pipe complete with spacers and end seals. The crown of the casing pipe is at elevation 230.63 m which corresponds to a depth of about 2.8 m below the center line of the railway tracks. The total length of trenchless pipe installation will be about 23 m, with a jacking/receiving pit at each end of the casing pipe.

The project site is located in the boulevard on the east side of Midland Street and starts approximately 25 to 30 m north of Saskatchewan Avenue. The test hole was drilled on the boulevard area directly west of the property at 5 Midland Street and approximately 16 m away from the CPR railway tracks. The area around the test hole and railway is generally flat lying. In the area of the proposed watermain renewal project there are overhead power lines and the existing watermain is located along the east side of Midland Street.

2) Field Investigation

On April 19, 2022, one test hole was drilled at the approximate location illustrated on Figure 1. The test hole was drilled by Paddock Drilling Ltd. using a truck mounted Acker MP8 drill rig equipped with 125 mm solid stem augers. The test hole was drilled to a depth of 6.1 m (20 feet) below grade.

The subsurface conditions were visually logged during drilling by DRI. Disturbed (auger cuttings) and undisturbed (Shelby tube) soil samples were recovered at regular depth intervals. The test hole was backfilled to grade with auger cuttings and bentonite chips. All samples were taken to DRI's Soils Testing Laboratory for additional visual classification and testing. The testing included determining the moisture contents of all samples and measuring bulk unit weights and undrained shear strengths on the Shelby tube samples. The test hole log in Appendix A summarizes the subsurface conditions encountered, results of

the laboratory testing and notes on the observations made during drilling. The UTM coordinates and ground elevation shown on the test hole log were surveyed by Tetra Tech.

3) Subsurface Conditions

The soil stratigraphy encountered in the test hole consists of clay fill, silt and silty clay. A general description of the main stratigraphic units is described below and is based on the test hole log in Appendix A. Refer to the test hole log for detailed information.

Clay Fill

A layer of clay fill was encountered at grade in the test hole. The clay fill is about 1.2 m thick and it contains trace to some sand and trace gravel. It is brown in color and wet with a soft to firm consistency. The moisture content of the clay fill is around 56 percent.

Silt

A silt layer was encountered at a depth of 2.1 m below grade. The silt layer is about 1.2 m thick and contains trace clay. It is light brown in color and is moist to wet with a loose compactness condition. The moisture content of the silt layer is around 27 percent.

Silty Clay

Lake Agassiz lacustrine silty clay was encountered beneath the clay fill layer at a depth of 1.2 m and beneath the silt layer at a depth of 3.3 m below grade. The upper layer of clay (above the silt layer) is approximately 0.9 m thick and it is brown in color, moist to wet with a stiff consistency and has high plasticity. The moisture content of the upper clay layer is around 40 percent.

The main deposit of silty clay below the silt layer is mottled brown and grey in color, moist with a firm to stiff consistency and it has high plasticity. The moisture content of the clay ranges from about 50 to 60 percent. The undrained shear strength of the clay was measured from the Shelby tube sample (T15), which was recovered at a depth of 4.6 m, using Torvane, penetrometer and unconfined compressive strength tests. The clay has undrained shear strengths ranging from about 30 to 60 kPa. The average bulk unit weight of the clay is around 16 kN/m³.

Glacial till was not encountered in the test hole however, local experience indicates that glacial till is present in the local area at a depth of approximately 10 m.

Test Hole Stability and Groundwater Conditions

In Winnipeg, groundwater usually occurs in shallow perched water tables within fill layers and silt deposits that are quite permeable and underlain by the relatively impermeable Agassiz clays. A groundwater table is not apparent during drilling within the clay soil due to its low permeability.

Trace groundwater seepage was observed from the clay fill layer below a depth of 0.6 m and from the silt layer. Sloughing of the silt layer was observed during drilling. Upon completion of drilling to a depth of 6.1 m, the test hole was open to 2.6 m and no water had accumulated above this depth. The groundwater conditions should be expected to vary seasonally, from year to year and possibly as a result of construction activities.

4) Discussion and Recommendations

Based on the attached test hole log and watermain crossing drawing prepared by Tetra Tech, which shows the top of casing pipe at elevation 230.63 m, the casing pipe will be located towards the bottom of the silt layer and the pipe invert should be a short distance into the underlying clay deposit. The silt layer encountered in the test hole is moist to wet and is susceptible to seepage and sloughing conditions. The extent of the silt layer (e.g. thickness and contact elevation) should be expected to vary along the length of the proposed trenchless pipe installation. The condition of the silt (e.g. moisture content) can vary along the length of the proposed casing pipe installation and seasonally, which will impact the groundwater seepage and sloughing potential of the layer.

Contractor bidding the casement pipe and carrier pipe installation work will need to select a trenchless excavation method that best suits the subsurface conditions expected in the work area and understanding that the subsurface conditions described on the test hole log in Appendix A can vary.

The potential for sulphate attack is considered to be severe (Exposure Class S-2). All concrete in contact with soil should be made with sulphate resistance cement (Type HS) in accordance with the current Manitoba Building Code and relevant CSA standards.

All excavation work should be completed by the Contractor in accordance with the current Manitoba Workplace Health and Safety Regulations to suit the planned and expected construction activities and schedule. Local excavations in fill materials may need to be flatter than allowed in the Manitoba Workplace Health and Safety Regulations. The earth pressure distribution shown on Figure 2 can be used for temporary braced shoring design.

5) Closure

This report and its findings were prepared based on the subsurface conditions encountered in the random representative test hole drilled on April 19, 2022 for the sole purpose of this geotechnical investigation and our understanding of the proposed watermain renewal project crossing the CPR Right-of-Way on Midland Street in Winnipeg, MB at the time of this report. Subsurface conditions are inherently variable and should be expected to vary across the site.

This report was prepared for the sole and exclusive use of Tetra Tech Canada Ltd. for the proposed watermain renewal project across the CPR Right-of-Way on Midland Street in Winnipeg, MB. The information and recommendations contained in this report are for the benefit of Tetra Tech Canada Ltd. only and no other party or entity shall have any claim against Dyregrov Robinson Inc., or the author, nor may this report be used for any other projects, including but not limited to changes in the proposed watermain renewal project without the consent of Dyregrov Robinson Inc. The findings and recommendations in this report have been prepared in accordance with generally accepted geotechnical engineering principles and practices. No other warranty, expressed or implied, is provided.

Please contact the undersigned if we can be of further assistance.

Sincerely,

DYREGROV ROBINSON INC.

Report Prepared By:

Report Reviewed By:

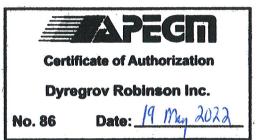
Alessandro Augellone, EIT

Geotechnical Engineering Intern

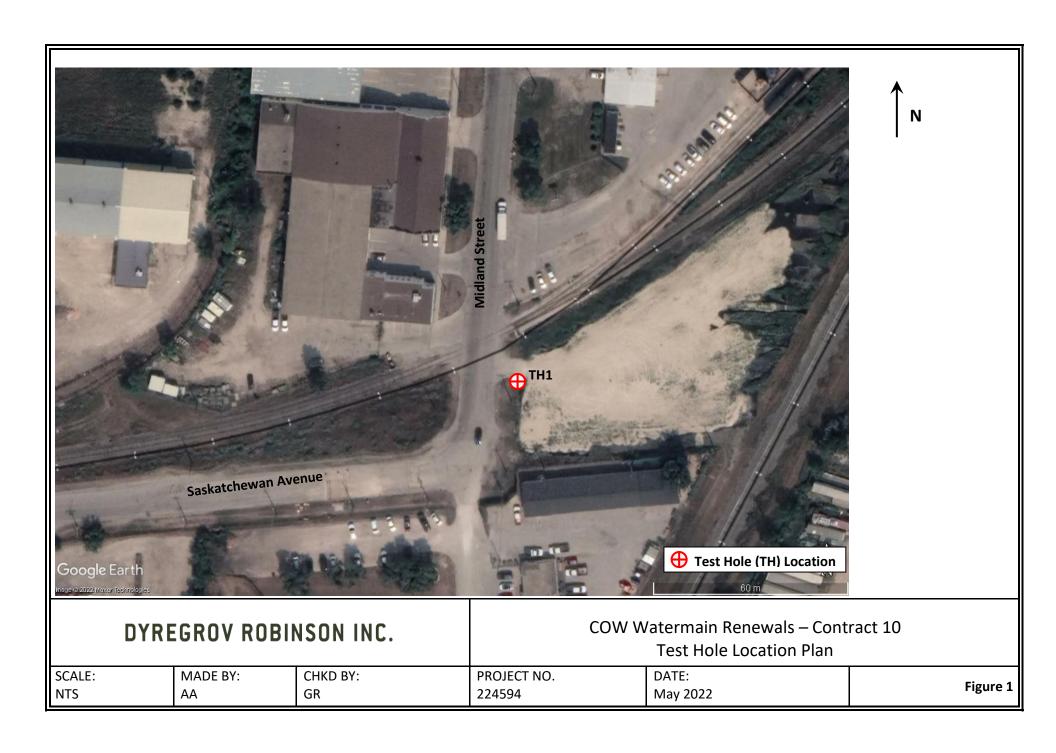
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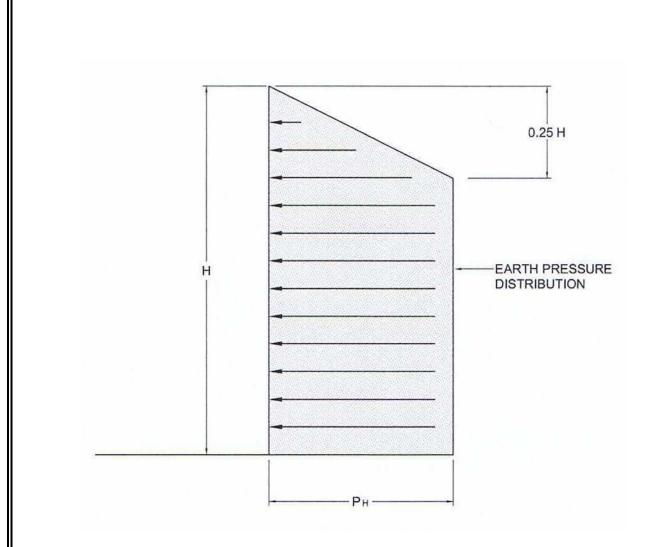
Gil Robinson, M.Sc., P.Eng.

Senior Geotechnical Engineer









$$Ph = 0.4 (\gamma H + q)$$

Where:

Ph = Lateral Earth Pressure (kPa)

 γ = Soil Unit Weight (17.3 kN/m³)

H = Depth of Excavation (m)

q = surface surcharge load (kPa)

DYREGROV ROBINSON INC.			EARTH PRESSURE DISTRIBUTION TEMPORARY BRACED SHORING		
SCALE:	MADE BY:	CHKD BY:	PROJECT NO.	DATE:	FIGURE 2
NTS	GR	AA	224594	May 2022	

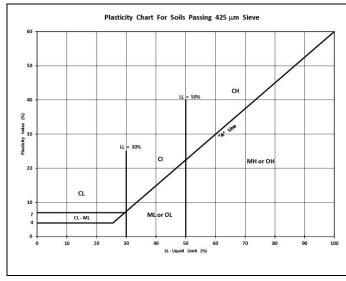
APPENDIX A

Test Hole Log

Tetra Tech Drawing: WM Crossing On Midland Street For CPR Approval

EXPLANATION OF TERMS & SYMBOLS

		_			TH Log	USCS		Laborator	y Classification Crite	eria
	Description				Symbols Classification	Fines (%)	Grading	Plasticity	Notes	
	GRAVELS (More than 50% of	CLEAN GRAVELS	Well graded sandy gravels or no f	s, with little	2727	GW	0-5	C _U > 4 1 < C _C < 3		
		(Little or no fines)	Poorly grade sandy gravel or no f	s, with little		GP	0-5	Not satisfying GW requirements		Dual symbols if 5-
SIIC	coarse fraction of gravel size)	DIRTY GRAVELS	Silty gravels, grave			GM	> 12		Atterberg limits below "A" line or W _P <4	12% fines. Dual symbols if above "A" line and
AINED SC		(With some fines)	Clayey grave sandy g			GC	> 12		Atterberg limits above "A" line or W _P <7	4 <w<sub>P<7</w<sub>
COARSE GRAINED SOILS		CLEAN SANDS	Well grade gravelly sand or no f	ls, with little	<u>0,00</u>	sw	0-5	C _U > 6 1 < C _C < 3		$C_{U} = \frac{D_{60}}{D_{10}}$
/O0	SANDS (More than 50% of	(Little or no fines)	Poorly grad- gravelly sand or no f	ls, with little	000	SP	0-5	Not satisfying SW requirements		$C_U = \frac{D_{60}}{D_{10}}$ $C_C = \frac{(D_{30})^2}{D_{10} x D_{60}}$
	coarse fraction of sand size)	action of	Silty sa sand-silt n			SM	> 12		Atterberg limits below "A" line or W _P <4	
			Clayey s sand-clay			SC	> 12		Atterberg limits above "A" line or W _P <7	
	SILTS (Below 'A' line W _L <50		Inorganic sil clayey fine s slight pla	ands, with		ML				
	negligible organic content)	W _L >50	Inorganic si plasti	•		МН				
SOILS	CLAYS (Above 'A' line negligible organic content) WL<30 WL<50 WL>50	W _L <30	Inorganic c clays, sand low plasticity,	y clays of		CL				
FINE GRAINED SOILS		30 <w<sub>L<50</w<sub>	Inorganic clay clays of n plasti	nedium		CI			Classification is Based upon Plasticity Chart	
FINE (W _L >50	Inorganic cla plasticity,			СН				
	ORGANIC SILTS & CLAYS	W _L <50	Organic s organic silty o plasti	clays of low		OL				
	(Below 'A' line) W _L >50		Organic cla plasti			ОН				
н	HIGHLY ORGANIC SOILS Peat and other highly organic soils			Pt		on Post fication Limit		r odour, and often s texture		
	Asphalt			Gl	lacial Till	^^^ / ^^^ /		edrock gneous)		
	Concrete			CI	ay Shale			edrock mestone)		ROBINSON INC. ECHNICAL ENGINEERS
X		Fill						edrock ferentiated)		



FRACTION			CLE SIZE	RELATIVE PR	
			Max.		Г
Bou	lders	>300		Percent	Descriptor
Cob	bles	75	300	>35%	main fraction
Gravel	Coarse	19	75	35 - 50	"and"
Glavei	Fine	4.75	19		
	Coarse	2.0	4.75	20 – 35	Adjective
Sand	Medium	0.425	2.0		e.g. silty, clayey
	Fine	0.075	0.425	10 – 20	"some"
Silt (non-plastic) or Clay (plastic)				10 – 20	Some
		< 0.0	075 mm	1 - 10	"trace"

Soil Classification Example

Clay 50% (main fraction), Silt 25%, Sand 17%, Gravel 8%

Clay – silty, some sand, trace gravel

TERMS and SYMBOLS

Laboratory and field tests are identified as follows:

Unconfined Comp.: undrained shear strength (kPa or psf) derived from unconfined compression testing.

Torvane: undrained shear strength (kPa or psf) measured using a Torvane

Pocket Pen.: undrained shear strength (kPa or psf) measured using a pocket penetrometer.

Unit Weight bulk unit weight of soil or rock (kN/m³ or pcf).

SPT – N Standard Penetration Test: The number of blows (N) required to drive a 51 mm O.D. split barrel sampler 300 mm into the soil using a 63.5 kg hammer with a free fall drop height of 760 mm.

DCPT Dynamic Cone Penetration Test. The number of blows (N) required to drive a 50 mm diameter cone 300 mm into the soil using a 63.5 kg hammer with a free fall drop height of 760 mm.

M/C insitu soil moisture content in percentPL Plastic limit, moisture content in percentLL Liquid limit, moisture content in percent

The undrained shear strength (Su) of cohesive soil is related to its consistency as follows:

Su (kPa)	Su (psf)	CONSISTENCY
<12	250	very soft
12 – 25	250 – 525	soft
25 – 50	525 – 1050	firm
50 – 100	1050 – 2100	stiff
100 – 200	2100 – 4200	very stiff
200	4200	hard

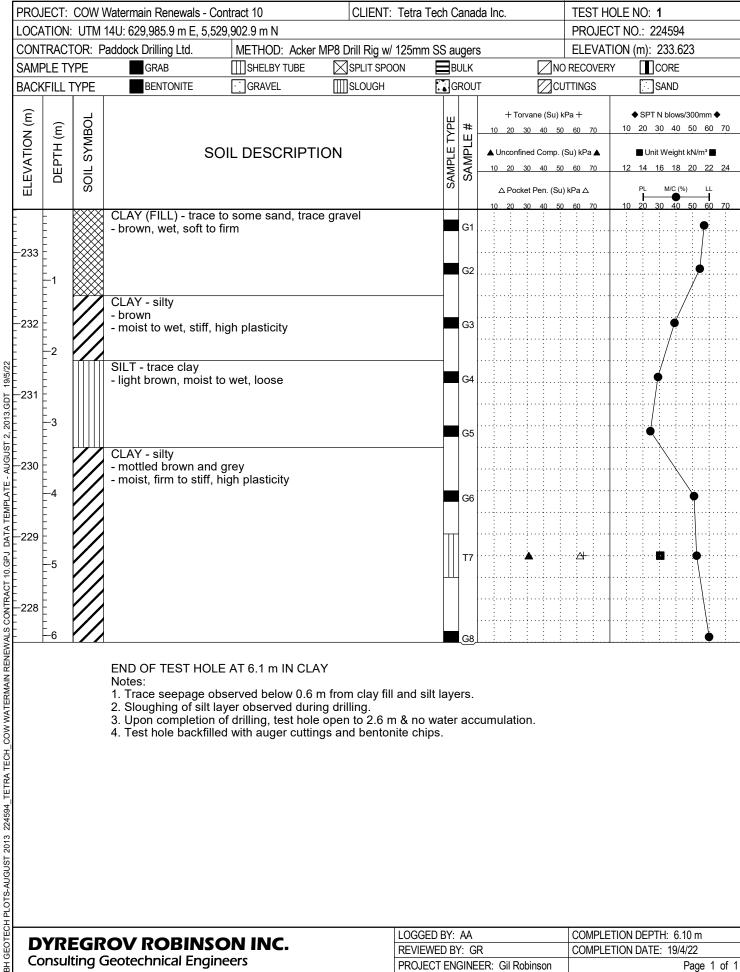
The SPT - N of non-cohesive soil is related to compactness condition as follows:

N - Blows / 300 mm	COMPACTNESS
0 - 4	very loose
4 - 10	loose
10 - 30	compact
30 - 50	dense
50 +	very dense

References:

ASTM D2487 - Classification of Soils For Engineering Purposes (Unified Soil Classification System)

Canadian Foundation Engineering Manual, 4th Edition, Canadian Geotechnical Society, 2006



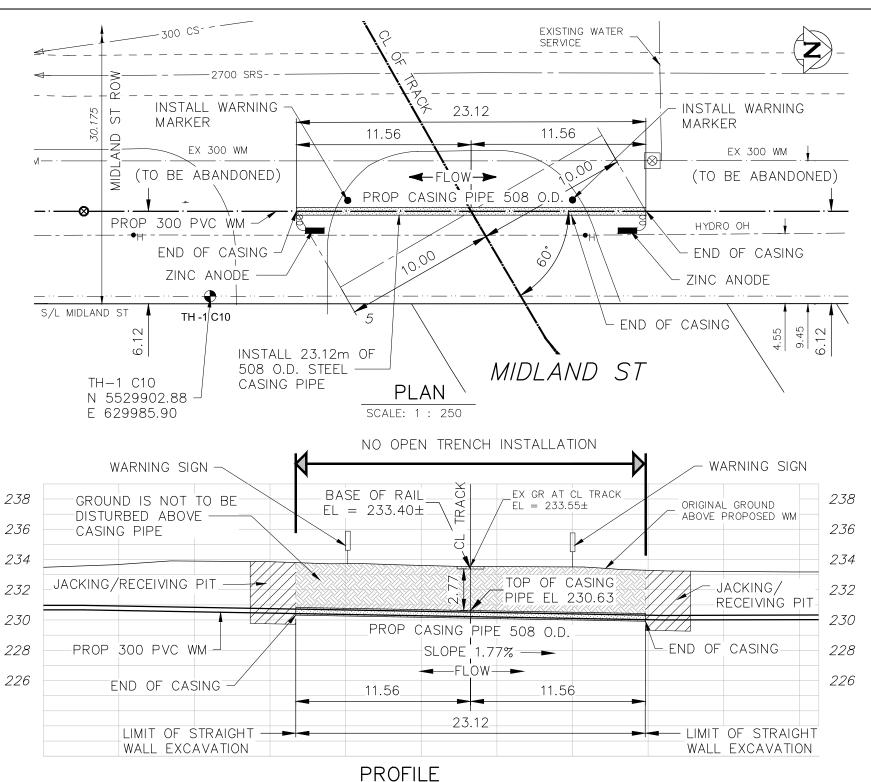
END OF TEST HOLE AT 6.1 m IN CLAY

Notes:

- Trace seepage observed below 0.6 m from clay fill and silt layers.
 Sloughing of silt layer observed during drilling.
- 3. Upon completion of drilling, test hole open to 2.6 m & no water accumulation.
- 4. Test hole backfilled with auger cuttings and bentonite chips.

DYREGROV ROBINSON INC.
Consulting Geotechnical Engineers

LOGGED BY: AA	COMPLETION DEPTH: 6.10 m
REVIEWED BY: GR	COMPLETION DATE: 19/4/22
PROJECT ENGINEER: Gil Robinson	Page 1 of 1

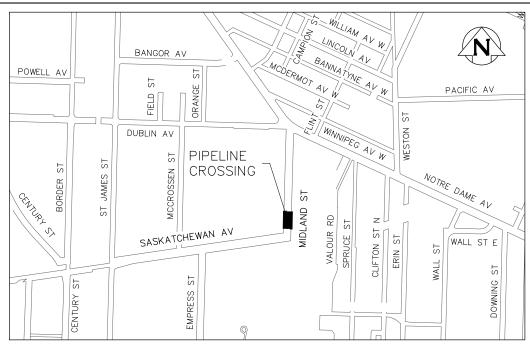


HOR & VERT SCALE: 1: 250 MATERIALS:

DESIGN NOTES:

- CROSSING TO BE DESIGNED, CONSTRUCTED, MAINTAINED AND OPERATED IN ACCORDANCE WITH TRANSPORT CANADA STANDARD (TCE – 10), STANDARDS RESPECTING PIPELINE CROSSING UNDER RAILWAYS
- 2. THE WATERMAIN CROSSINGS UTILIZE CASING PIPES DESIGNED TO THE GUIDELINES SPECIFIED IN THE AREMA MANUAL OF RAILWAY ENGINEERING CHAPTER 1 PART 5 "PIPELINES".

- 1. CARRIER PIPE POTABLE WATER PIPE PVC AWWA C-900 CLASS 150 (DR18)
- 2. ENCASEMENT PIPE SHALL CONFORM TO ASTM A53 STEEL PIPE, ASTM SPECIFICATIONS A134 MILD CARBON STEEL, A139, GRADE B. BUTT WELD JOINTS SHALL HAVE A MINIMUM THICKNESS OF 13mm REGARDLESS OF DIAMETER. NO COATING
- 3. ENCASEMENT PIPE SPACERS SHALL BE 200MM WIDE, HEAVY DUTY TWO PIECE STAINLESS STEEL BANDS WITH 25mm WIDE BY 75mm SPACERS, EQUAL TO ADVANCE PRODUCTS AND SYSTEMS INC. (APS) MODEL SS18.
- 4. ENCASEMENT PIPE SEALS SHALL BE WRAPAROUND RUBBER WITH STAINLESS STEEL BAND CLAMPS AND WATERPROOF MASTIC SEALS SPACERS EQUAL TO ADVANCE PRODUCTS AND SYSTEMS INC. (APS) MODEL AW OR AZ.
 5. SACRIFICIAL ANODE — 10.9 kg ZINC ANODES AT EACH END OF CASING PIPE.



LOCATION PLAN

SCALE: 1: 15000

PIPE SPECIFICATIONS						
PIPE	OUTSIDE DIAMETER	CDECIFICATION COMMENTS		COMMENTS		
CARRIER PIPE	335MM	19MM	PVC DR 18 BELL & SPIGOT (WATERMAIN)	WORKING PRESSURE — 450 kPa/ TESTED AT 1034 kPa		
CASING PIPE	508MM	15MM	CARBON STEEL ASTM A53 SCHEDULE 40 — JOINT WELD	TRENCHLESS INSTALLATION		
SPACERS			SS BANDS, POLYMER RUNNERS (APS MODEL SSI)	YES SEE NOTES: MATERIAL 3.		
END SEALS			RUBBER (APS MODEL AW)	YES SEE NOTES: MATERIAL 4.		
CATHODIC PROTECTION		10.9 kg ZINC ANODES	YES SEE NOTES: MATERIAL 5.			

CONSTRUCTION NOTES:

- 1. CONSTRUCTION IN ACCORDANCE WITH TRANSPORT CANADA STANDARD (TCF-10)
- 2. CASING PIPE WILL BE INSTALLED USING TRENCHLESS METHODS BY HORIZONTAL EARTH CORING.
- 3. THE WATERMAIN PIPE WILL BE INSERTED INTO THE CASING PIPE COMPLETE WITH SPACERS AND END SEALS.
- 4. EMERGENCY VALVE LOCATIONS FOR THE 300mm WATERMAIN (36.8 M NORTH & 14.1 M SOUTH).



WM CROSSING ON MIDLAND STREET FOR CPR APPROVAL

AUTHORIZED BY: IJM	CLIENT DRAWING NO.		
DATE: 22/05/	1		
DESIGNED BY: SJR	DRAWN BY: NL/SJR	DRAWING NO.	REV.
REVIEWED BY: IJM	SCALE: 1:250	2200120200-SKT-C0001	0